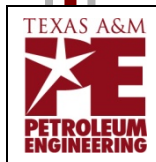


Extending Shale Gas Well Life with Low Grade Geothermal Power

Srikanth Thoram
Dr. Christine Ehlig-Economides
Texas A&M University, College Station

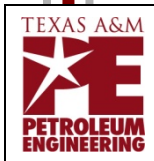
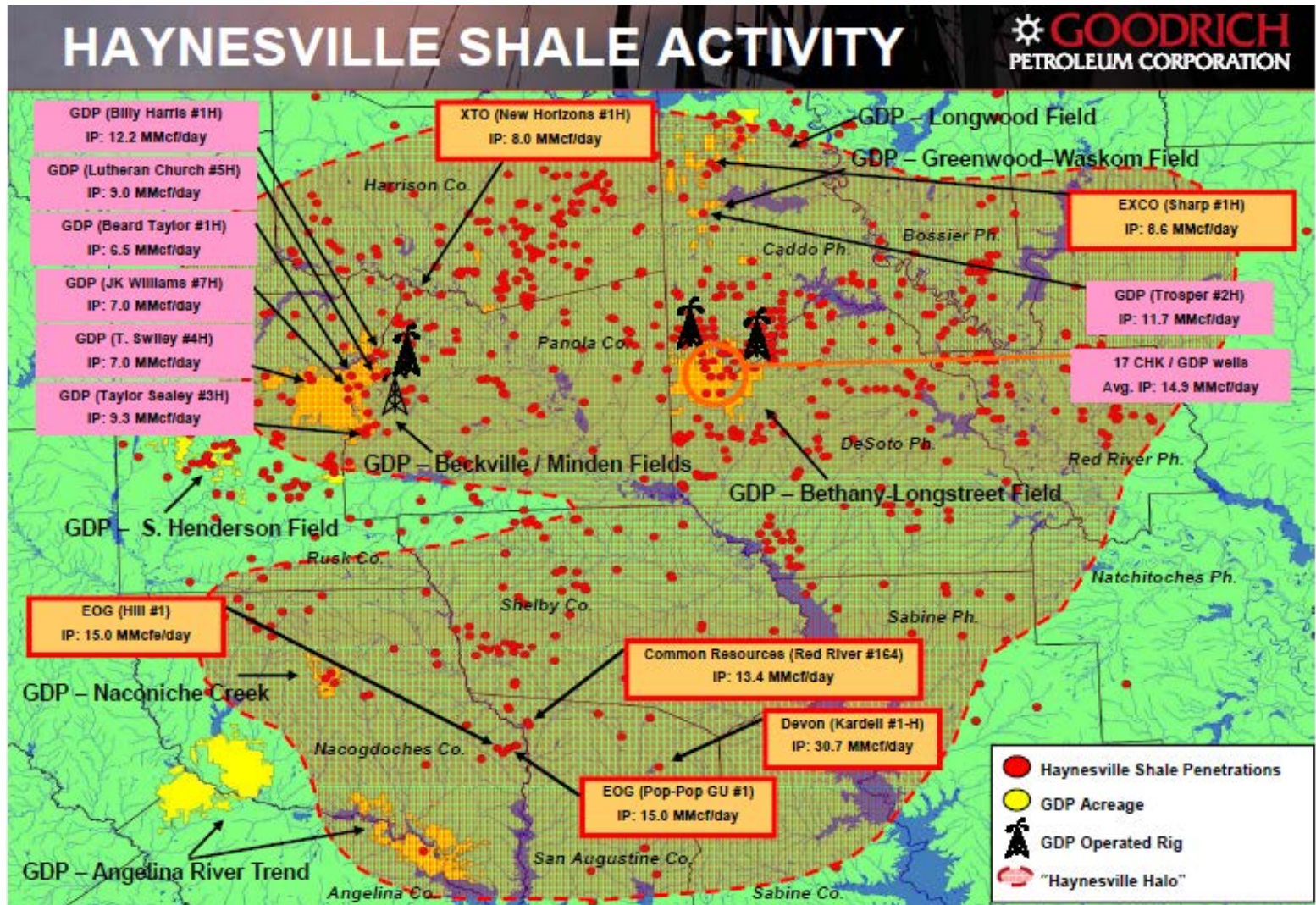


October 25th, 2011

Agenda

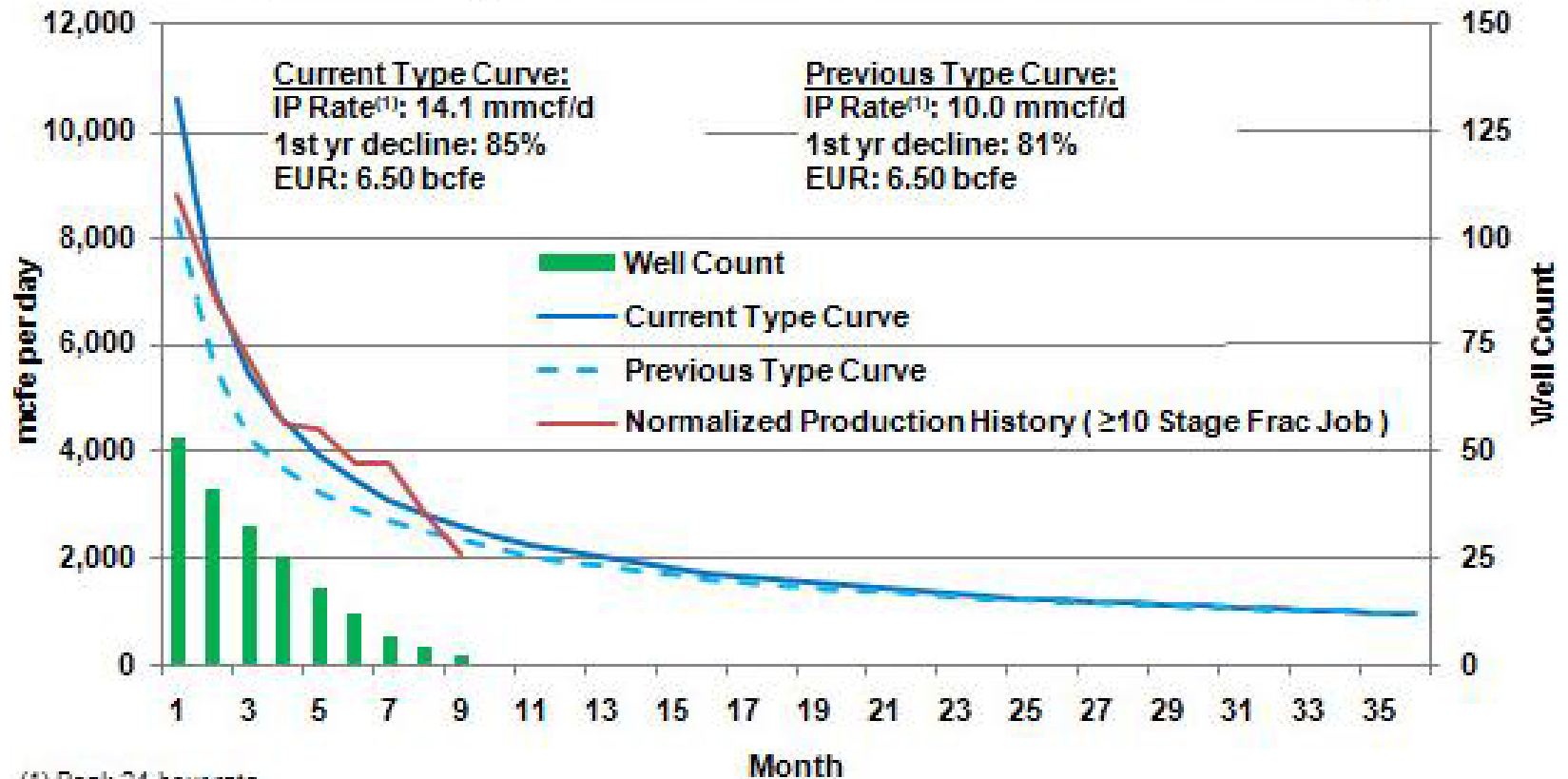
- Introduction
- Models for geothermal heat extraction
- Geothermal Power Plant
- Project Economics
- Conclusions and recommendations
- Future work

Haynesville Shale

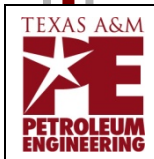


Haynesville Production Behavior

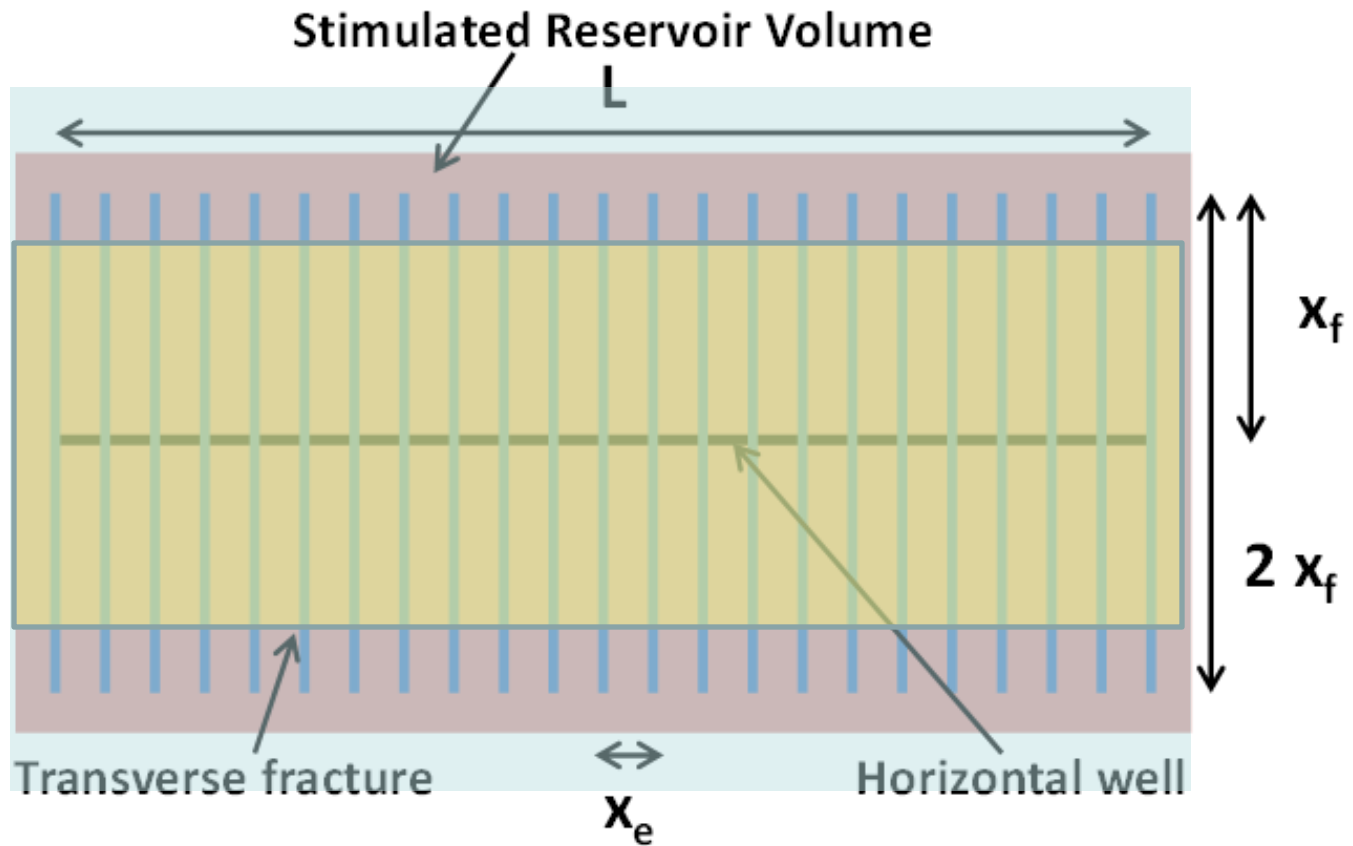
Haynesville Type Curve and Normalized Production History



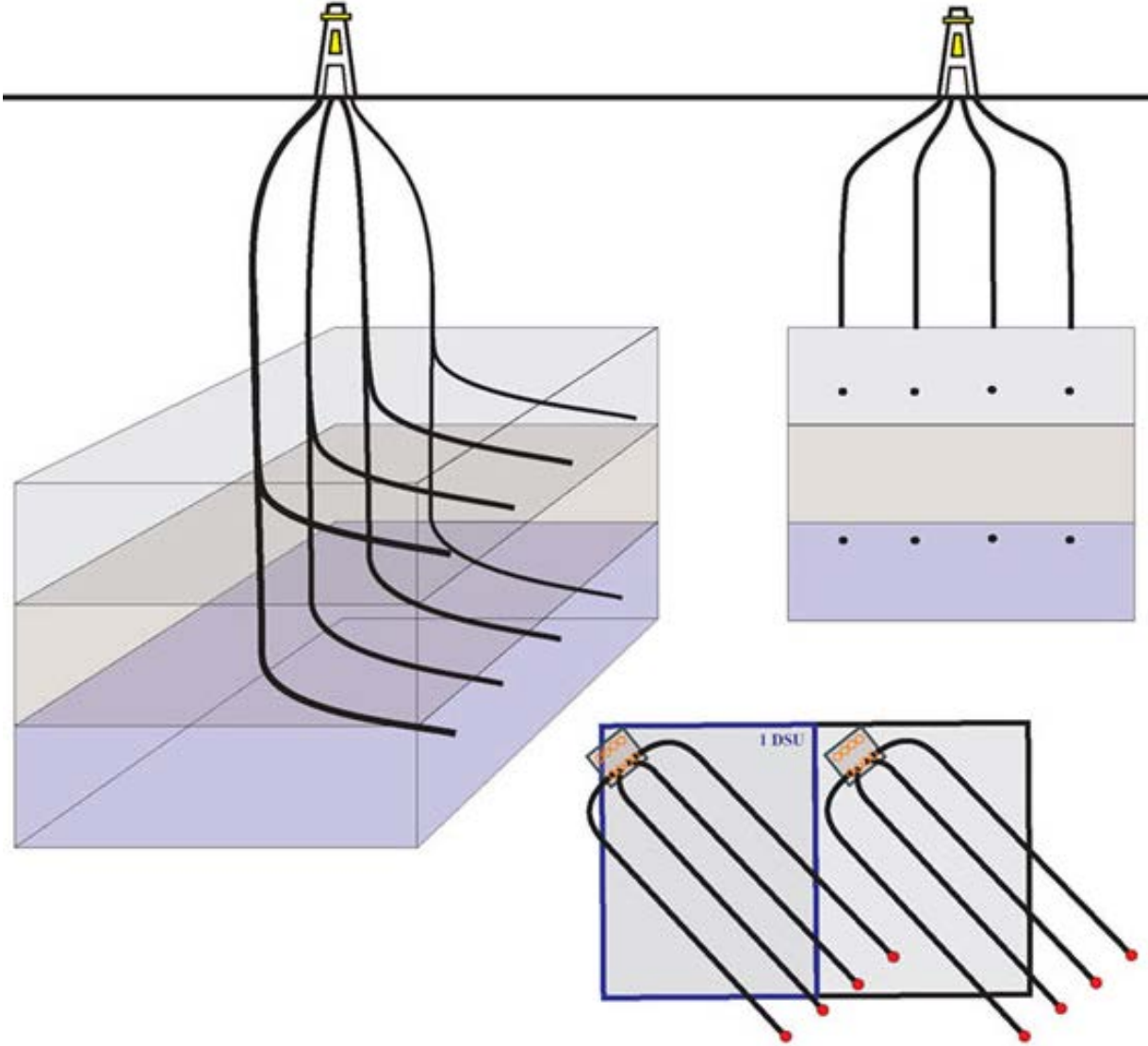
(1) Peak 24-hour rate



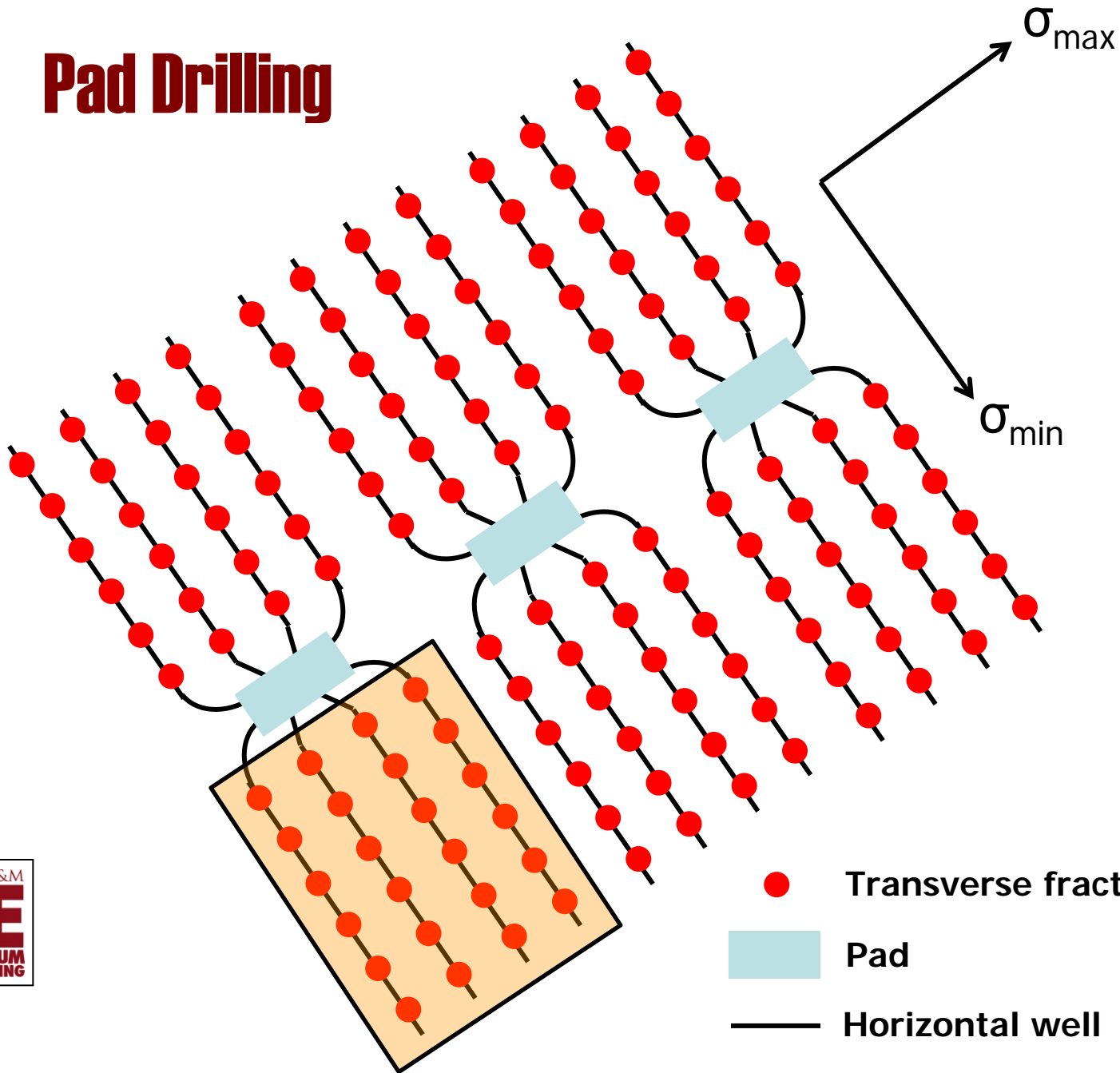
Planar view of the Stimulated Reservoir Volume



Pad Drilling

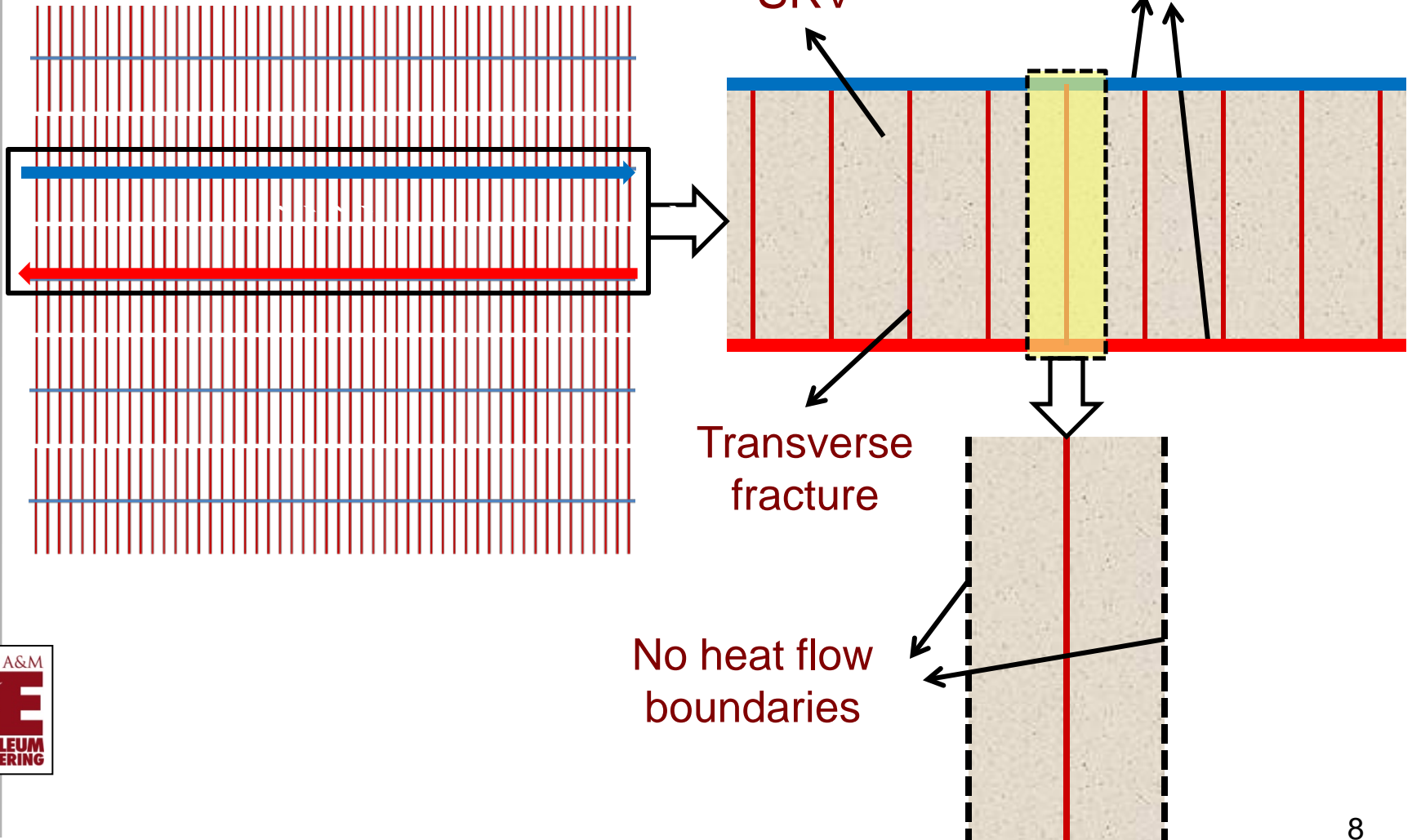


Pad Drilling

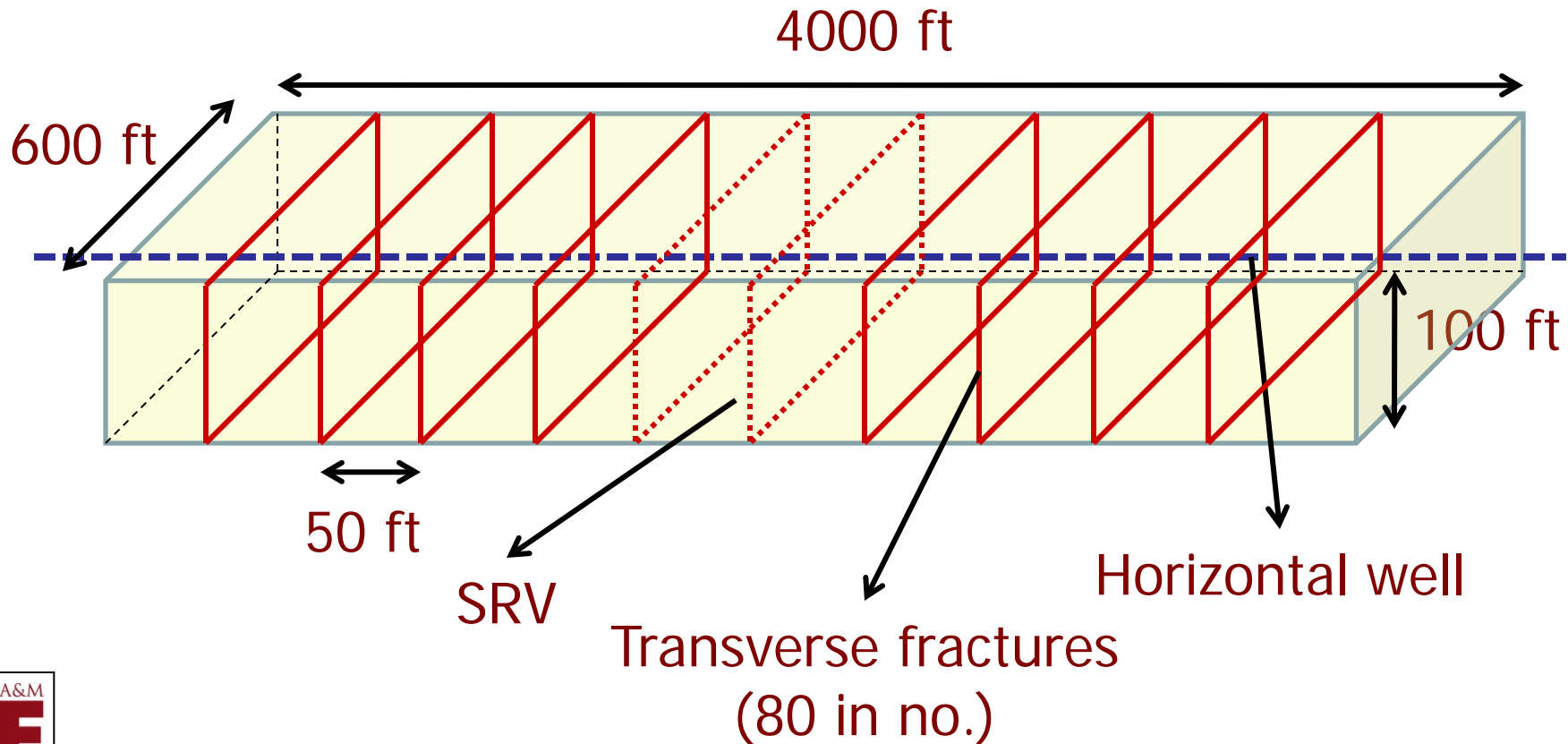


Idealization of Haynesville Shale Gas Well

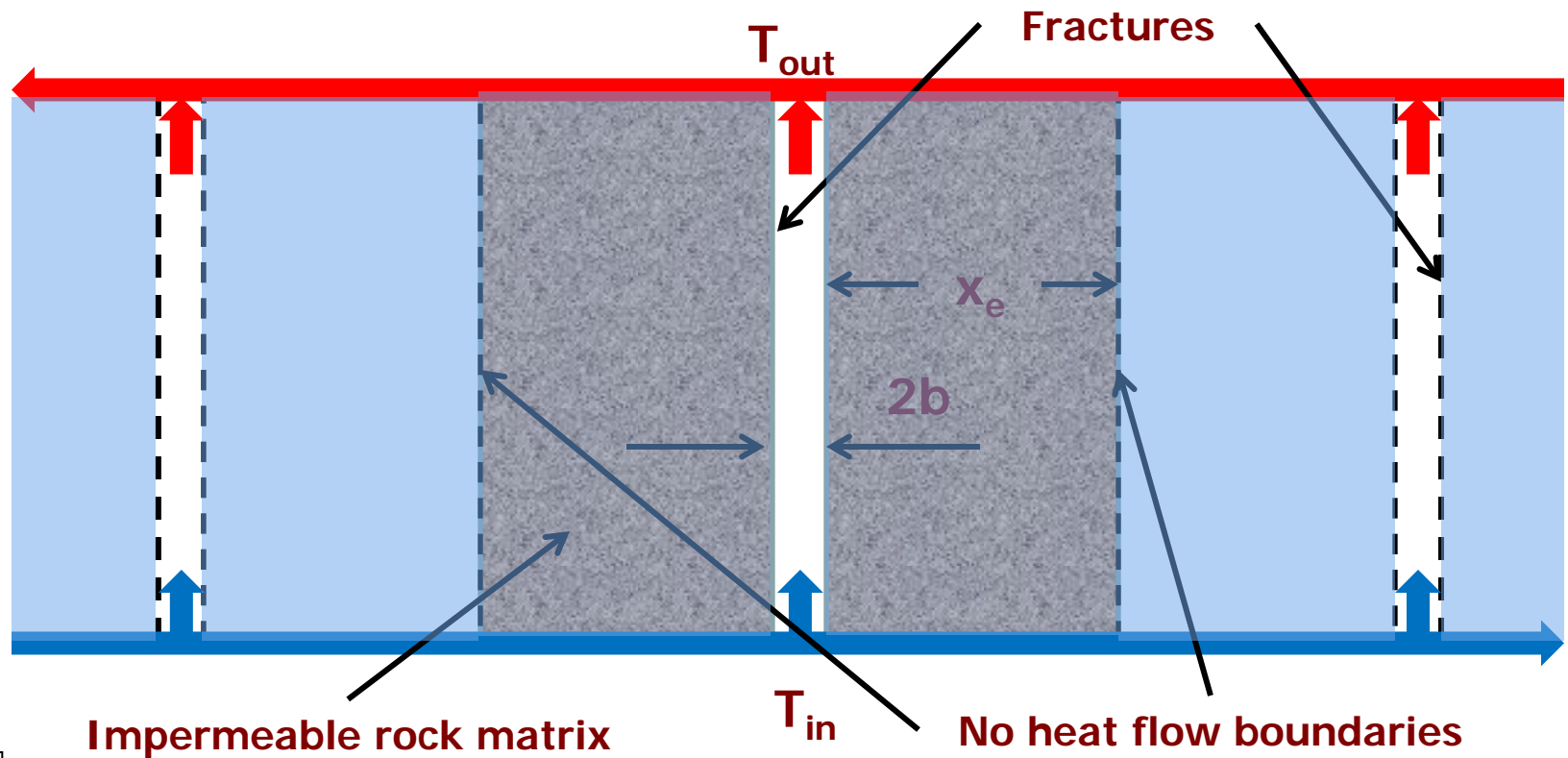
Array



Typical SRV dimensions of a Shale Gas well in Haynesville



Analytical Model



Analytical Model

Heat conduction in rock matrix

$$\frac{\partial^2 T_r(x, y, t)}{\partial x^2} = \frac{\rho_r c_r}{k_r} \frac{\partial T_r(x, y, t)}{\partial t}$$

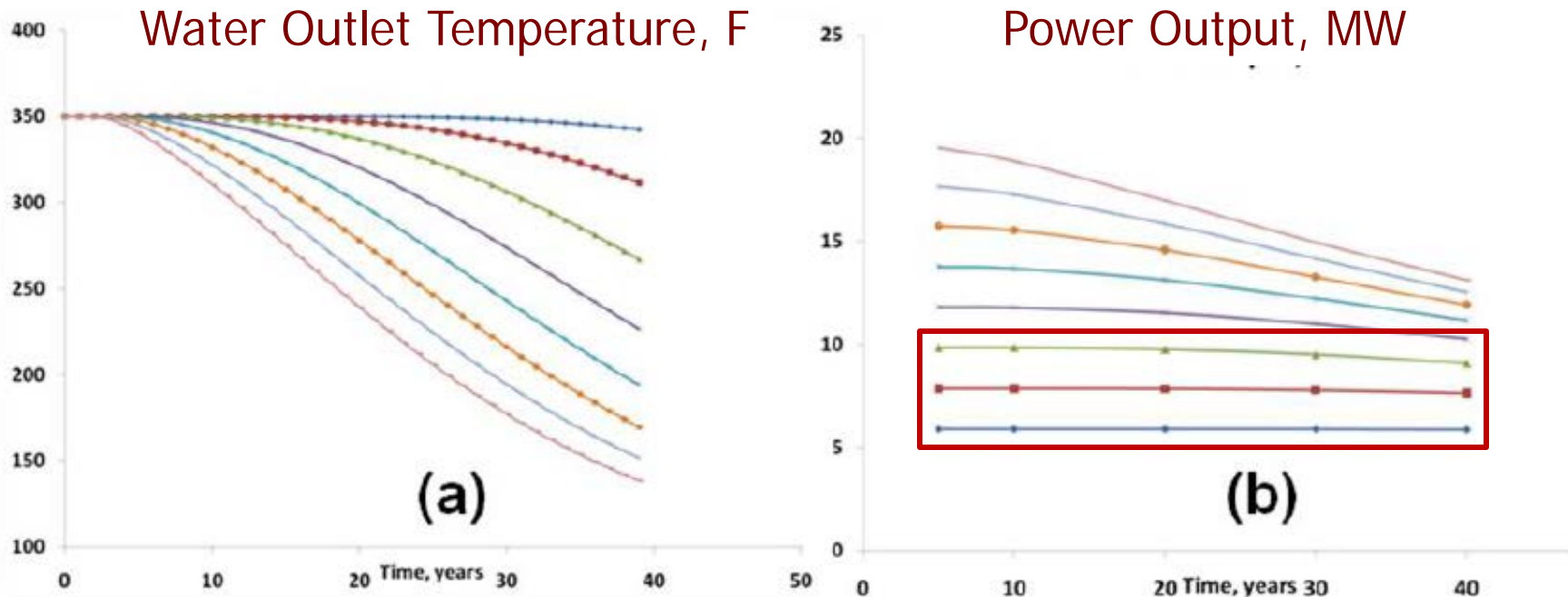
Heat conduction and convection for water in fracture

$$b\rho_w c_w \left[\frac{\partial T_w(y, t)}{\partial t} + v \frac{\partial T_w(y, t)}{\partial y} \right] = k_r \frac{\partial T_r(x, y, t)}{\partial x} \quad (\text{at } x=b)$$

Laplace transform solution

$$T_{wD}(y_D, s) = \frac{1}{s} \text{Exp}[-y_D s^{\frac{1}{2}} \tanh\left(\frac{Q\rho_w c_w x_e}{2 k_r y_f}\right) s^{\frac{1}{2}}$$

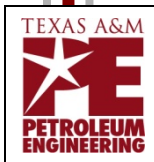
Sensitivity to injection rate per fracture



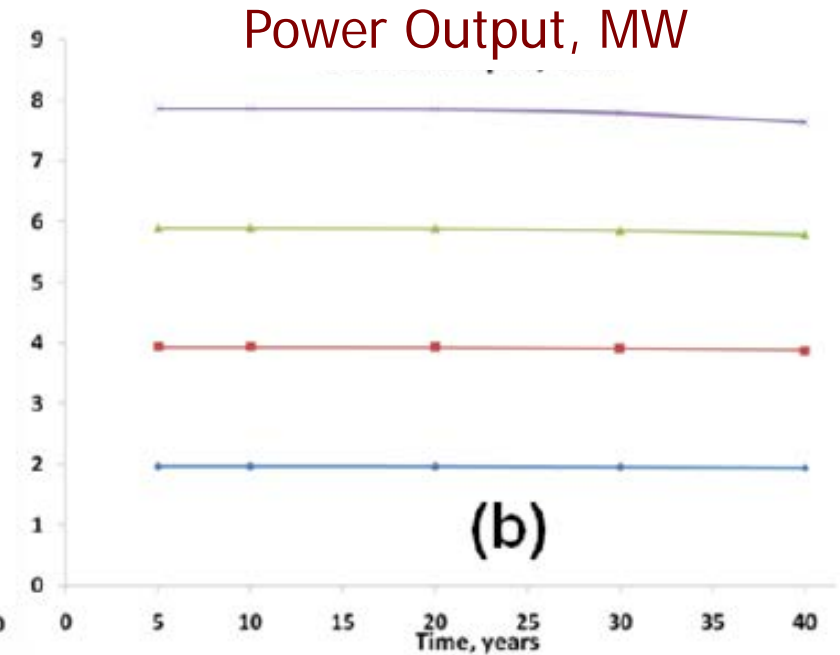
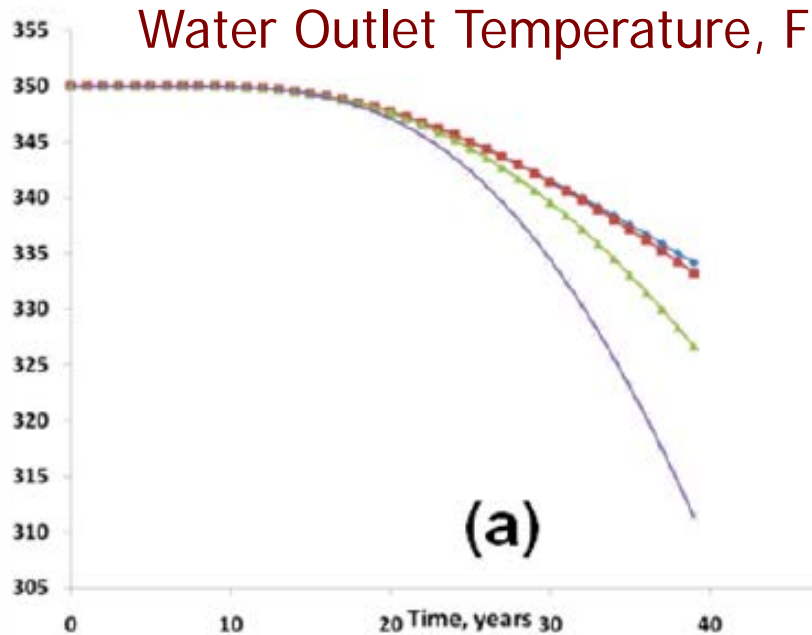
Injection flow rate per fracture, bbl/day

—●— 30
 —■— 40
 —▲— 50
 —✱— 60
 —✱— 70
 —◆— 80
 —◆— 90
 —■— 100

80 fractures, 50 ft. spacing



Sensitivity to number of fractures



No. of fractures, fracture spacing, ft.

◆ 20, 200

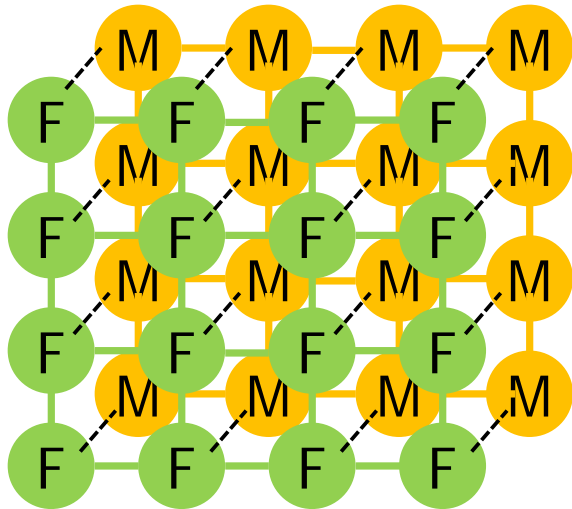
■ 40, 100

▲ 60, 66.67

✕ 80, 50

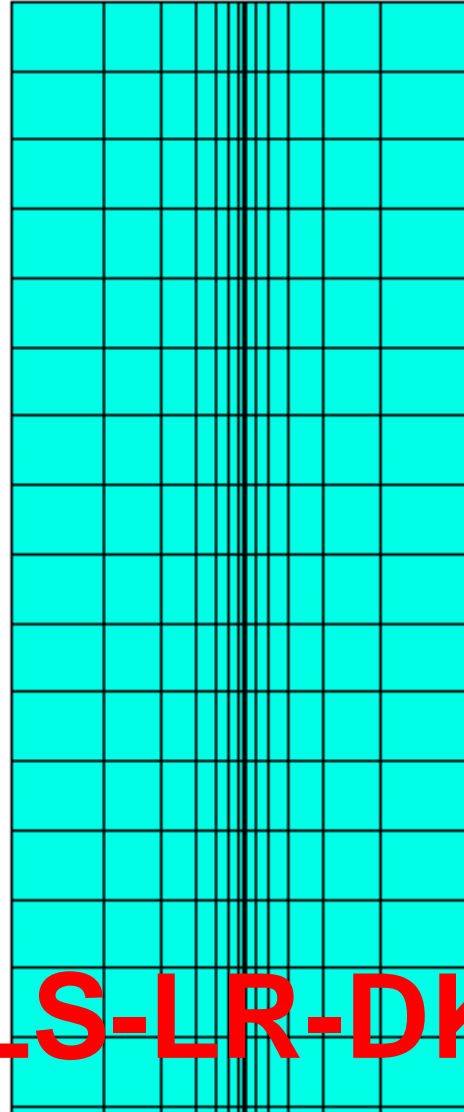
Injection flow rate per fracture = 40 bbl/day

Dual permeability (DK) and MINC models

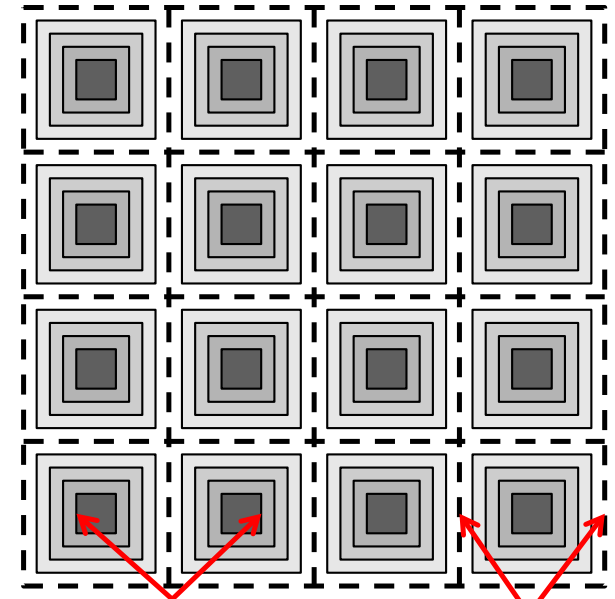


F Fracture block
M Matrix block

DK



LS-LR-DK



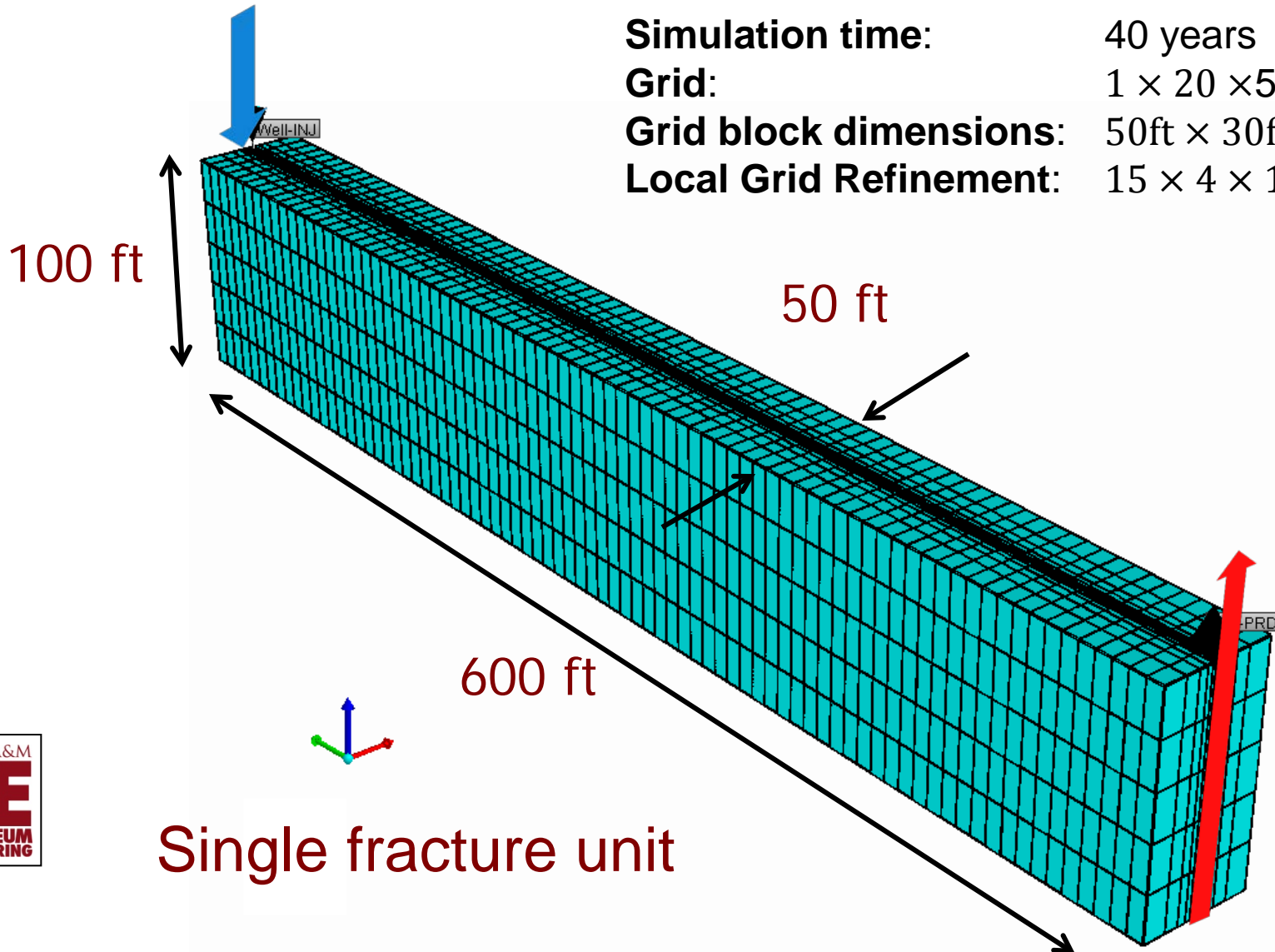
Subgridding of matrix blocks

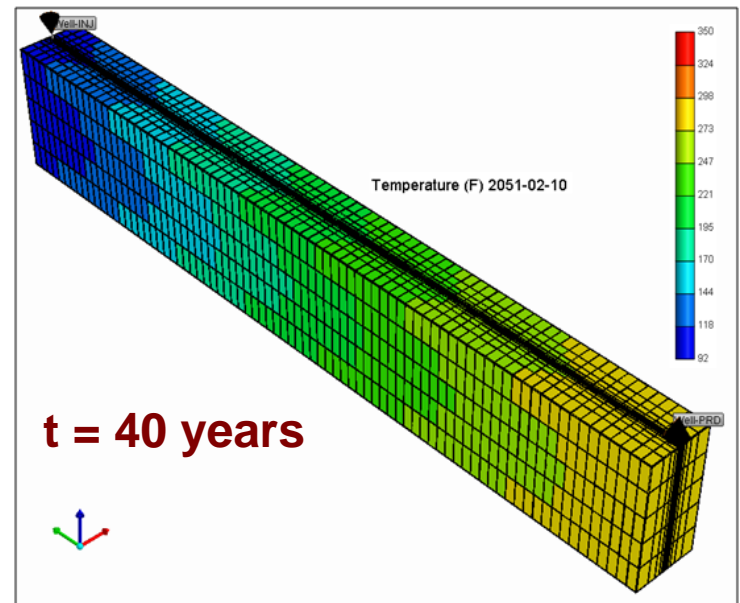
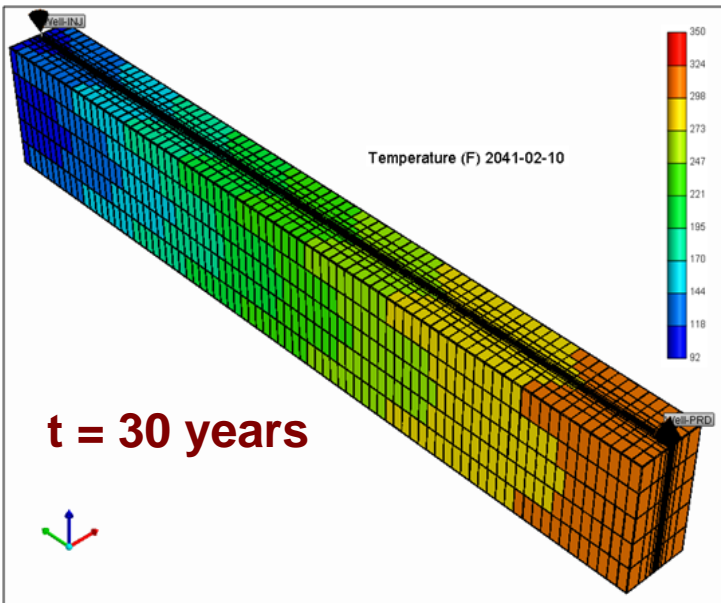
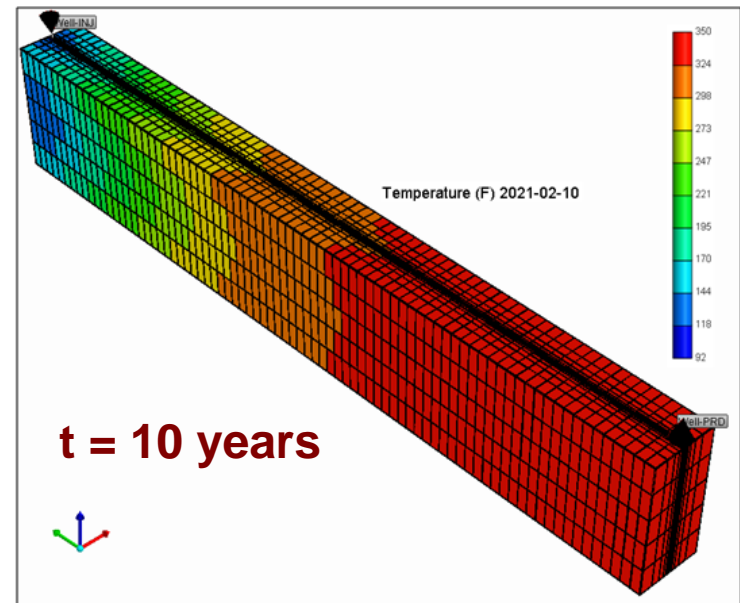
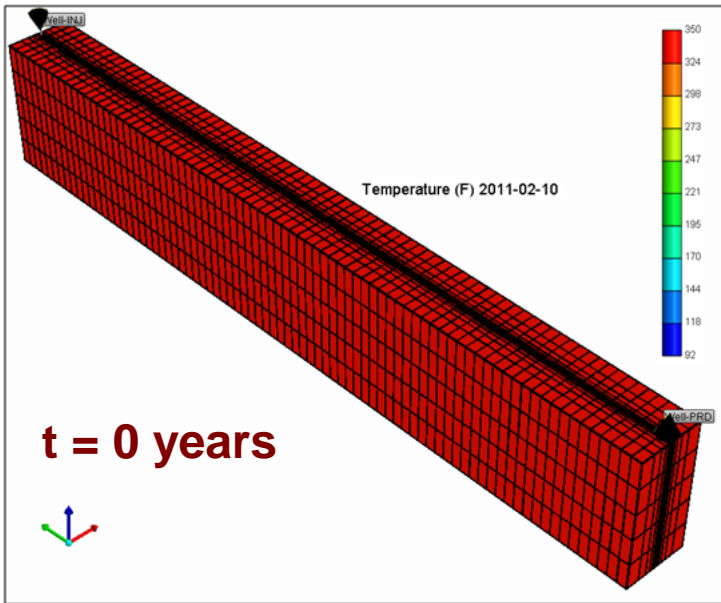
Fractures

MINC

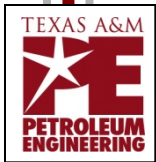
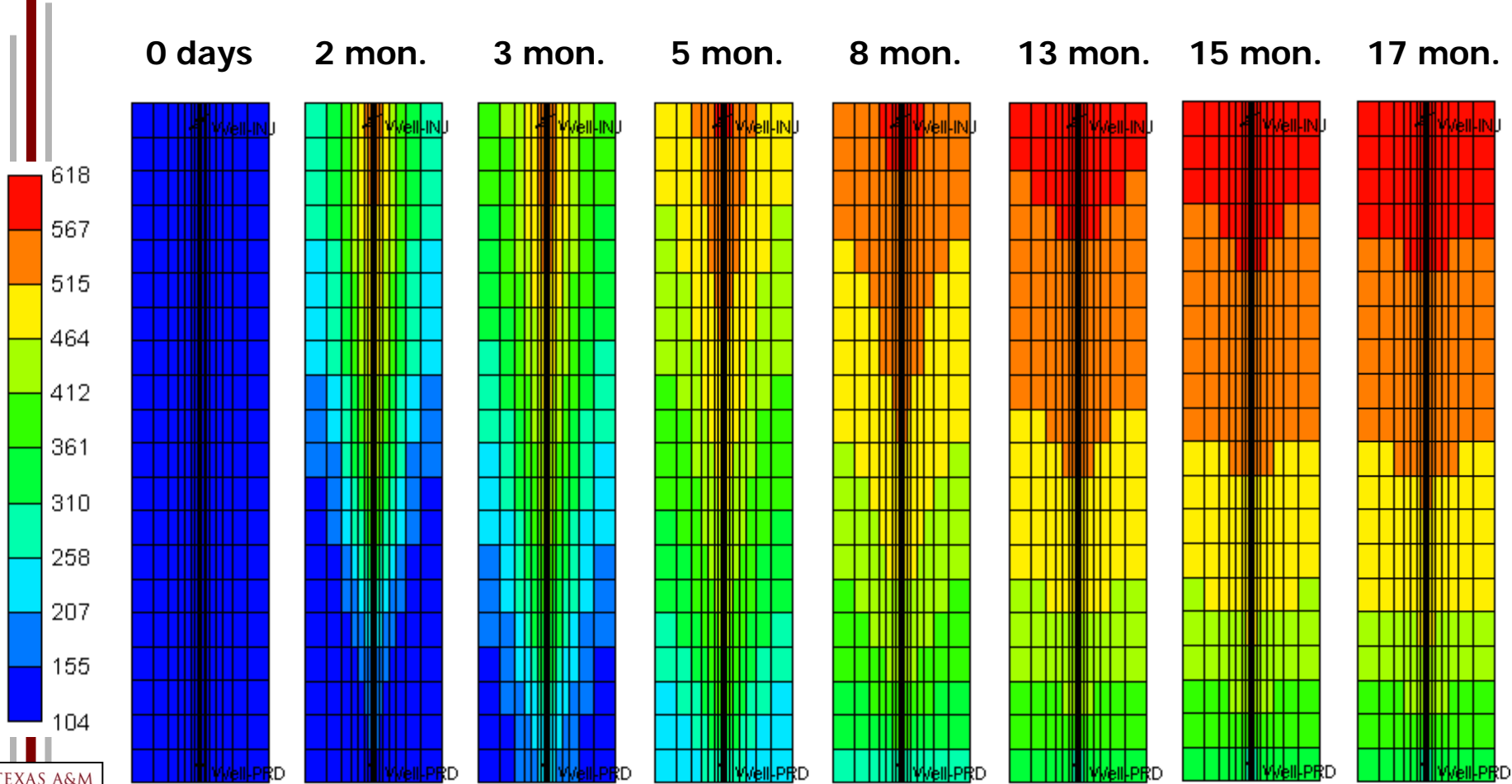
Numerical Model – CMG

Simulation time: 40 years
Grid: $1 \times 20 \times 5$
Grid block dimensions: 50ft \times 30ft \times 20ft
Local Grid Refinement: $15 \times 4 \times 1$



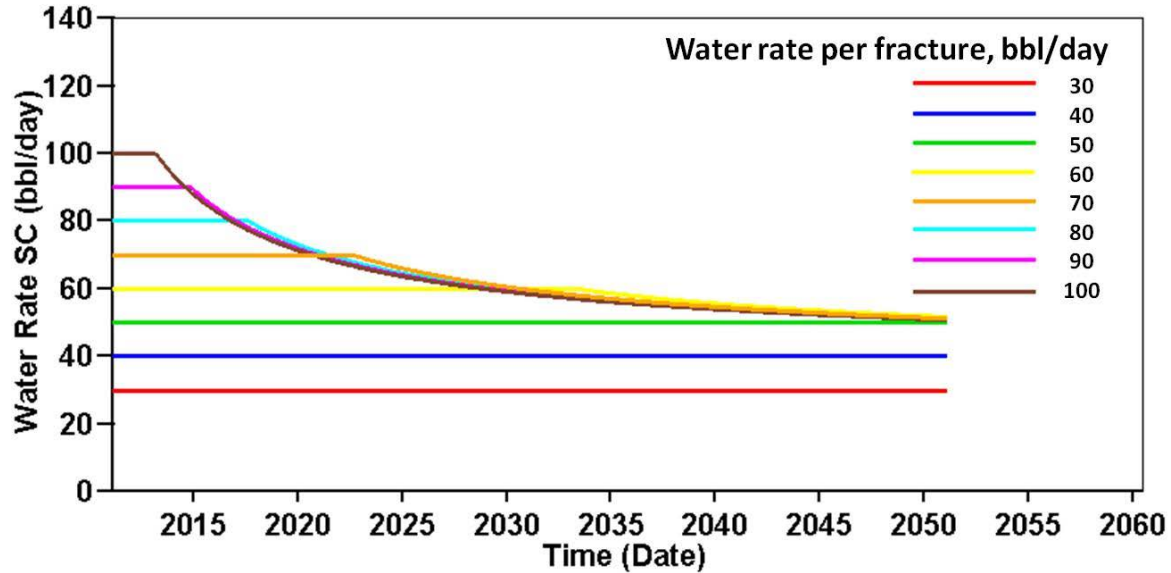


Thermal front movement

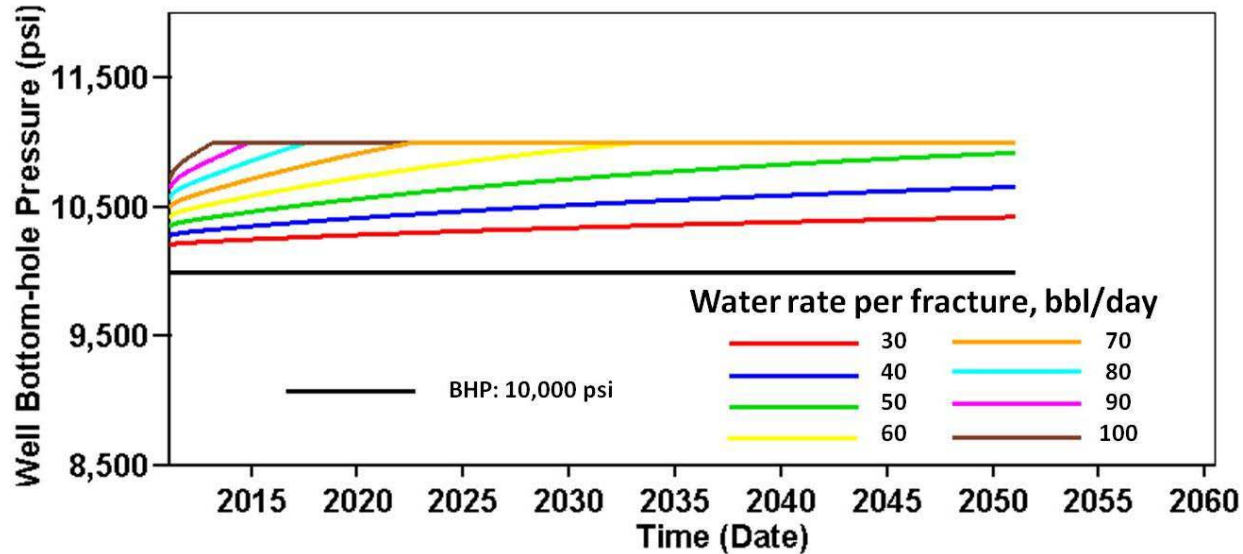


Simulation Results

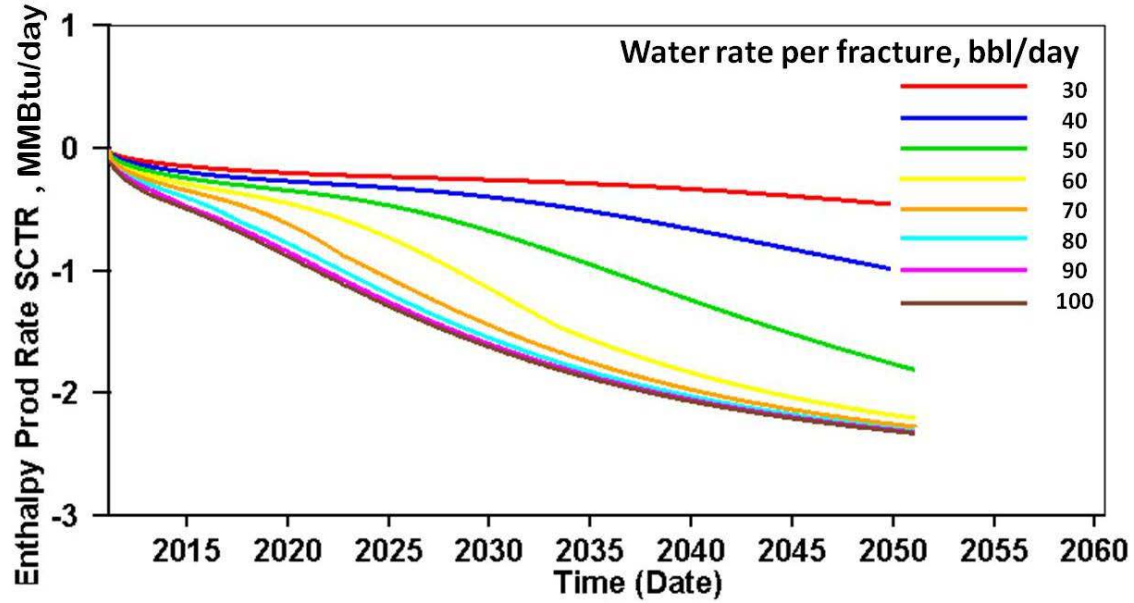
Injection rate per fracture, bbl/day



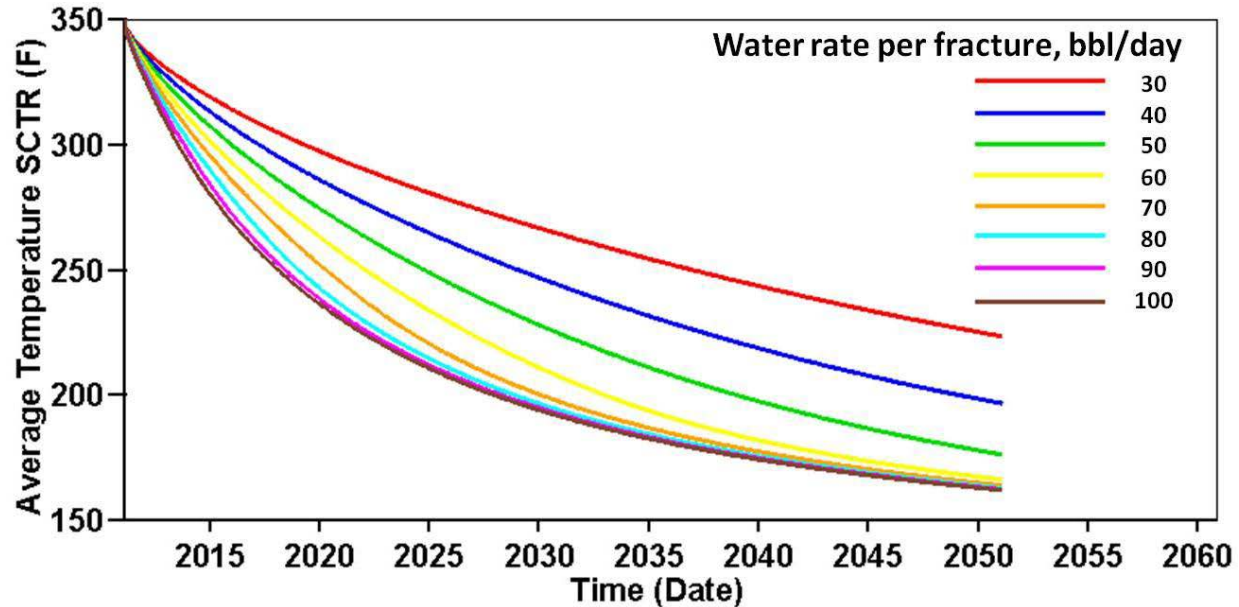
Well Bottom-hole Pressure, psia



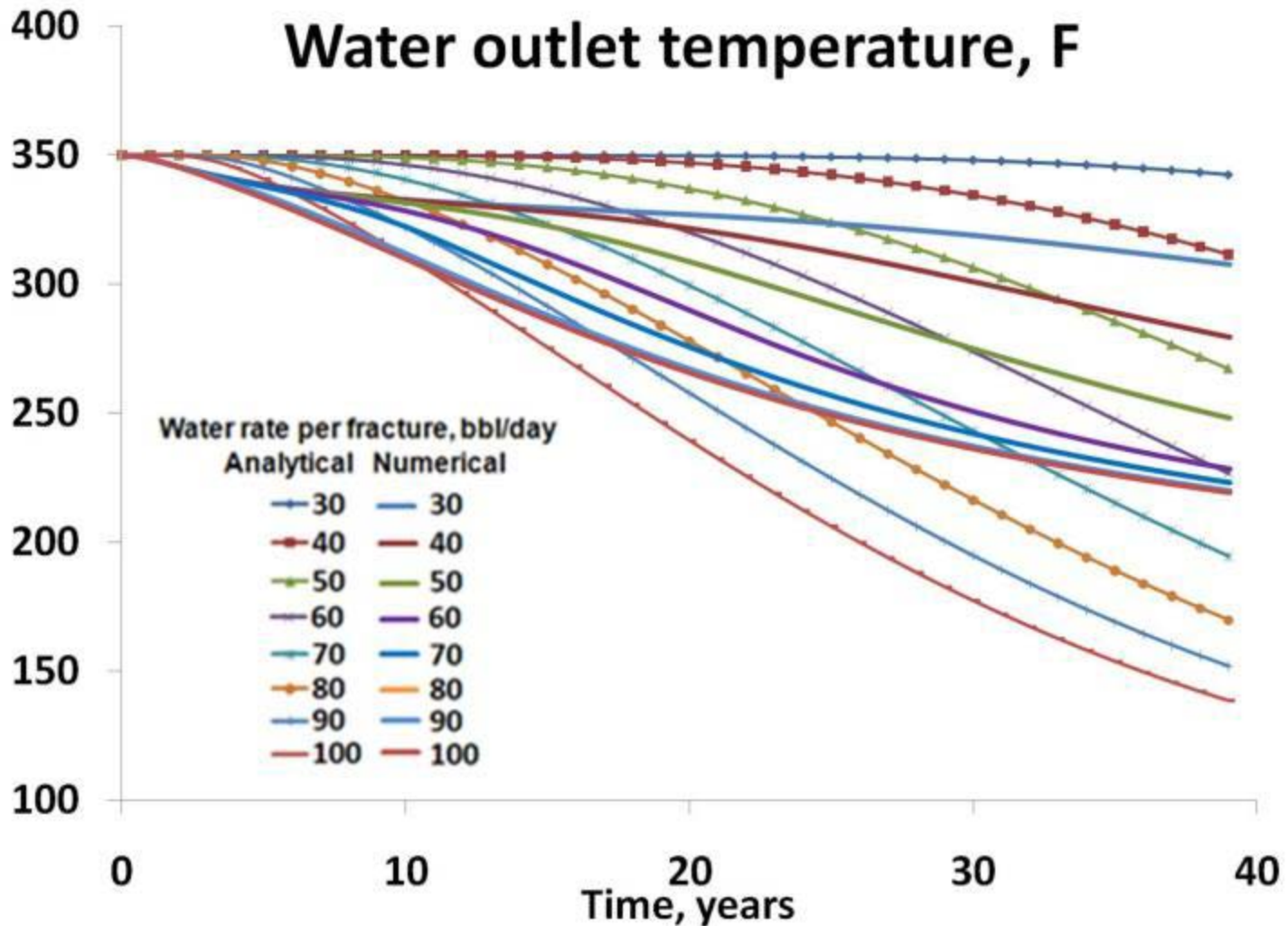
Enthalpy Production Rate, MMBtu/day



Average Formation Temperature, F

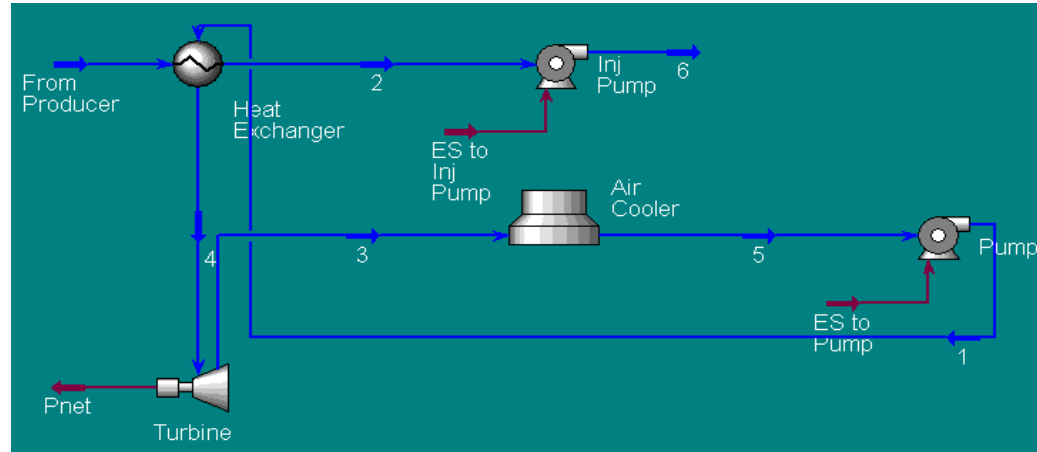


Water outlet temperature

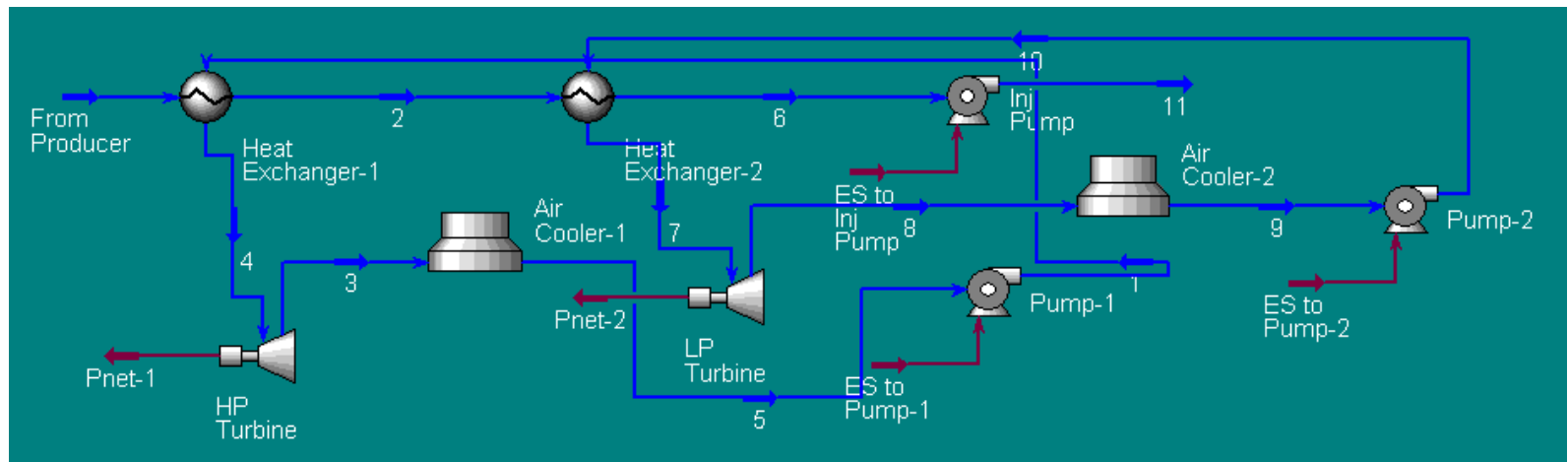


Binary Cycle Power Plant

AspenHYSYS

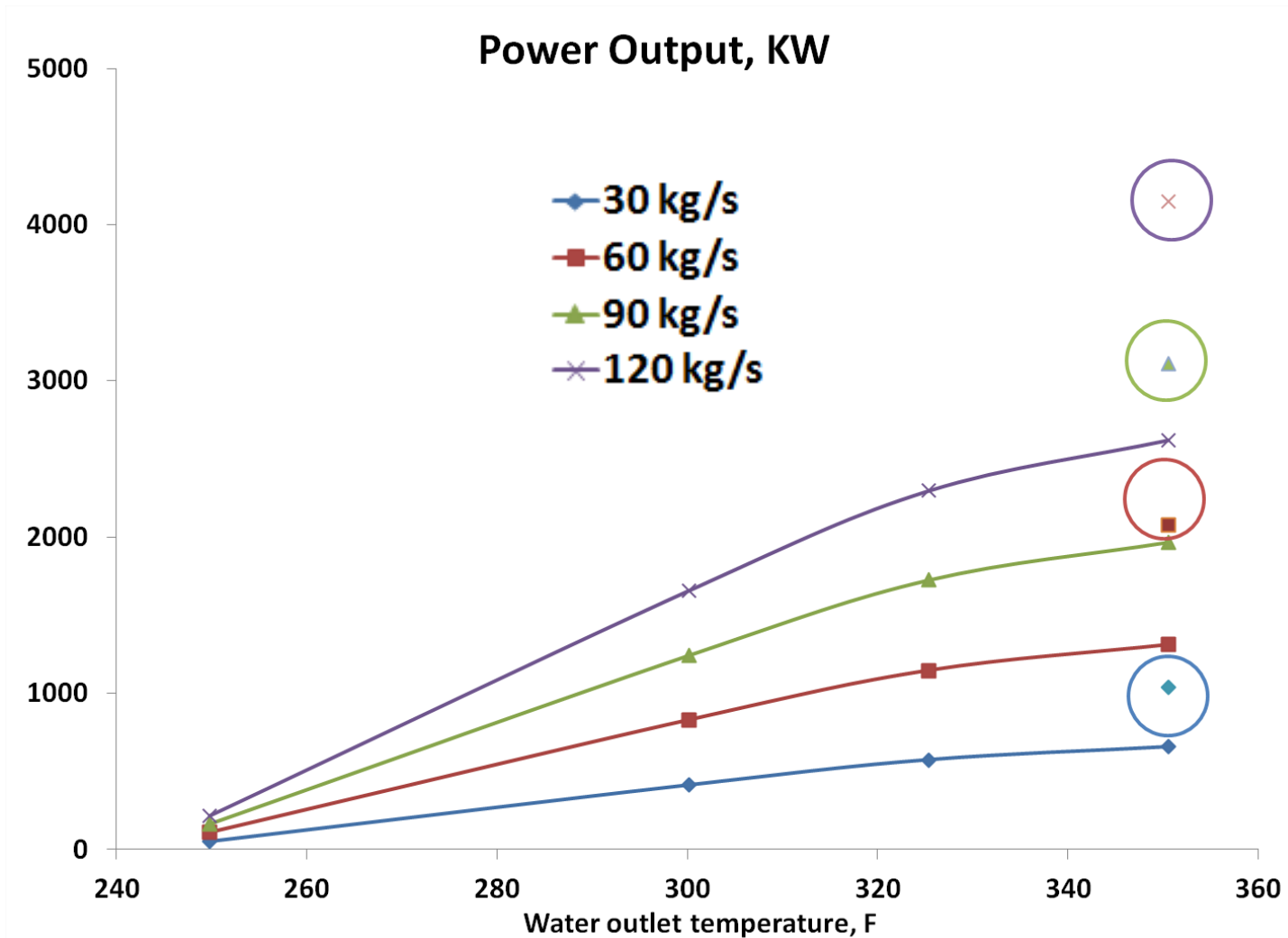


Basic Binary Power Plant

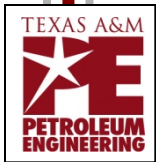
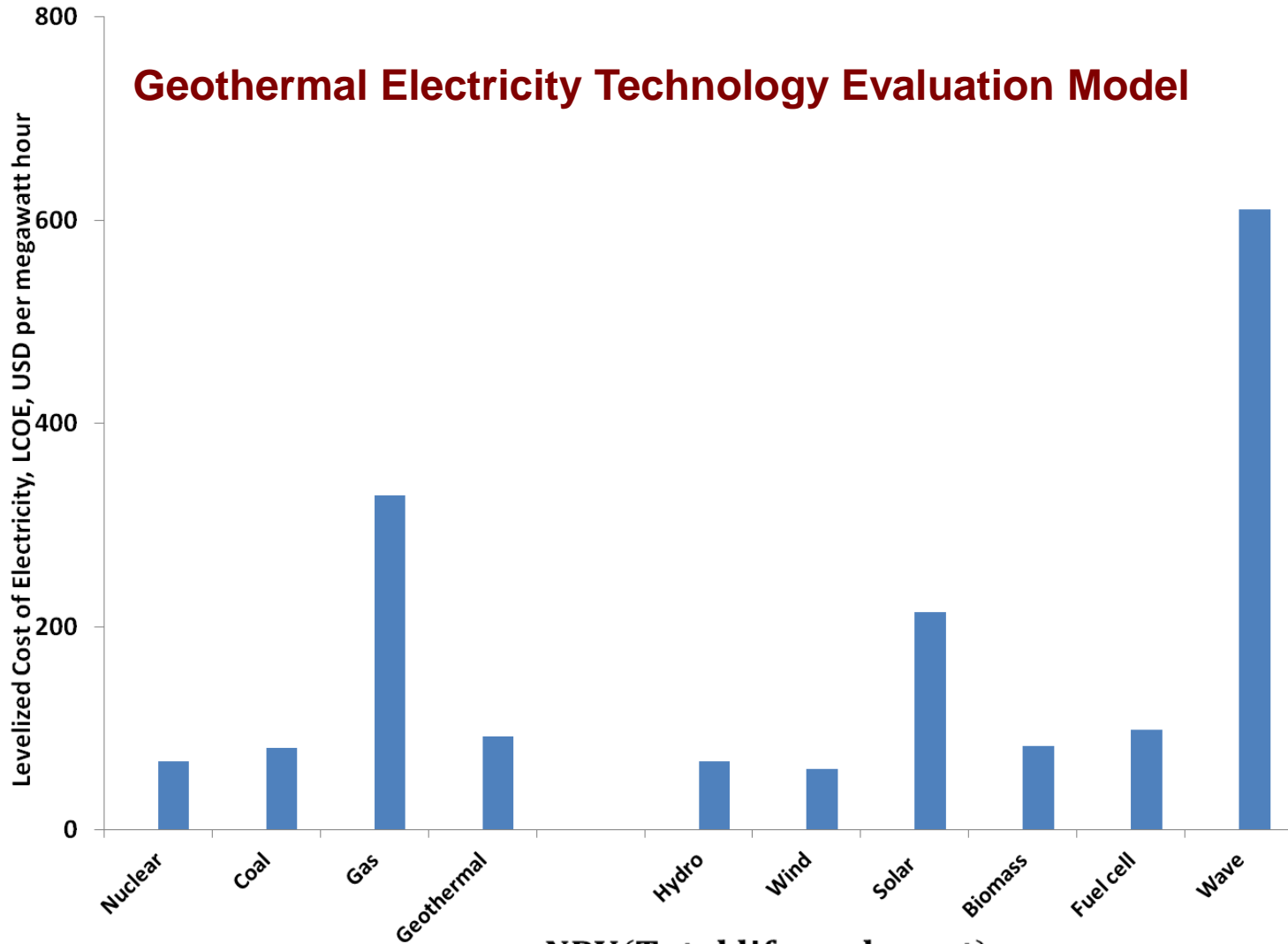


Dual Pressure Binary Cycle Power Plant

Net Power comparison for different water flow rates

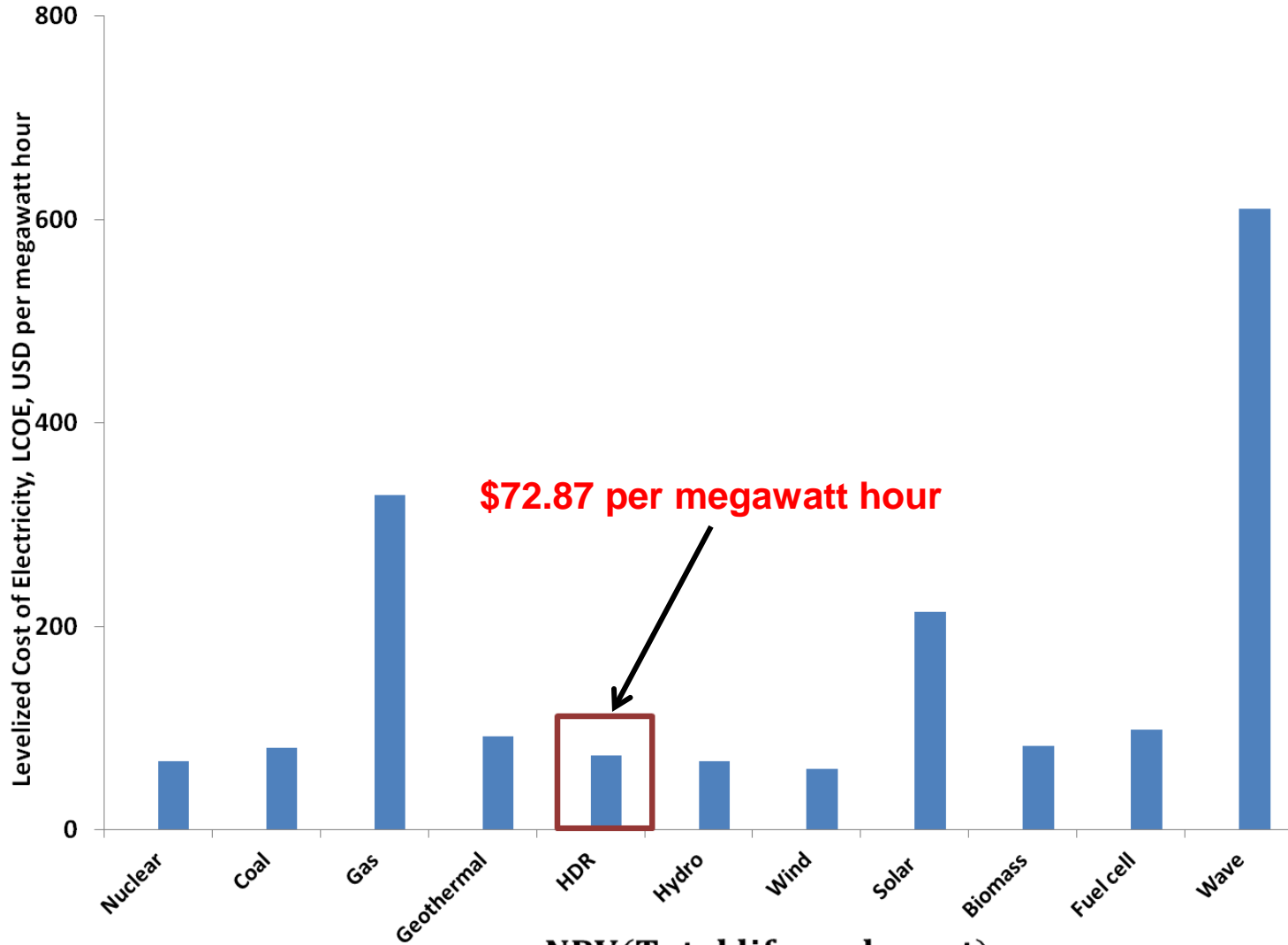


Economics – LCOE Comparison

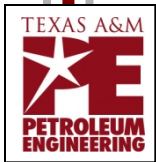


$$\text{LCOE} = \frac{\text{NPV}(\text{Total life cycle cost})}{\text{Total lifetime energy production}}$$

Economics – GETEM Model



$$\text{LCOE} = \frac{\text{NPV}(\text{Total life cycle cost})}{\text{Total lifetime energy production}}$$



Conclusions & Recommendations

- Coupling models with a surface binary cycle power plant suggests that reuse of Haynesville shale gas production wells for low grade geothermal heat extraction after gas production is depleted appears feasible both technically and economically.
- Sufficient connectivity between adjacent wells can greatly aid to project economics by eliminating well drilling and completion costs.

Conclusions & Recommendations

- Dual pressure binary plant is more efficient and results in higher power output.
- Estimated LCOE of \$73 per megawatt hour compares favorably to a natural gas power plant.

Future work

- Develop generalized intergranular thermo-geomechanical-chemical coupled model.
- Thermal contraction of the rock results in increased power output and should be incorporated into the model.